Amendments

In the Specification:

Please amend the paragraph starting at p. 12, line 20, as follows:

Figs 3a and 3b show (to an exaggerated degree in the drawing) the changes in the angle α and β respectively subtended between successive card flat clothings 18a, 18b, 18c and the tangent to the cylinder clothing 4a. According to Fig. 3a, the pins $14b_1$, $14b_3$ and $14b_5$ lie on the sliding-contact surface 21a of the ~~first~~ second slideway 21 and the pins $14b_2$, $14b_4$ and $14b_6$ lie on the sliding-contact surface 20a on the ~~second~~ first slideway 20. ~~The sliding-contact surface 20a, partly visible in side view, is drawn with a broken line and the visible sliding-contact surface 21a is drawn with a continuous line.~~ The distance between the tip circle 22 of the cylinder clothing 4a and the sliding-contact surface 20a is denoted by the reference c_1 and the distance to the sliding-contact surface 21a by the reference c_2. The distance c_2 is larger than the distance c_1. The clothing 14d of the card flat bars 14^I, 14^{II}, 14^{III} forms a respective acute angle a with the tangent to the cylinder clothing 4a, with the result that the carding nip narrows in the direction of rotation 4b of the cylinder 4. The distance between the clothing 14d and the cylinder clothing 4a is denoted at the entry of the carding nip by the letter d, and at the exit by the letter a, d being greater than a. The angle of inclination a is termed the so-called offset angle. The slow-running card flat bars 14^I, 14^{II}, 14^{III} are located in the region of the card flat guide roller 13a, that is, in the region of the card flat exit or fibre intake.

Please amend the paragraph starting at p. 13, line 17, as follows:

Referring to Fig. 3b, the pins $14b^8$, $14b^{10}$, $14b^{12}$ lie on the sliding-contact surface 20a of the ~~second~~ first slideway 20 and the pins $14b^7$, $14b^9$ and $14b^{11}$ lie on the sliding-contact surface 21a on the ~~first~~ second slideway 21. ~~The sliding-contact surface 21a, visible in side view, is drawn with a continuous line and the partly visible sliding-contact surface 20a is drawn with a broken line.~~ The distance between the tip circle 22 of the cylinder clothing 4a and the sliding-contact surface 21a is denoted by the reference c_3 and the distance to the sliding-contact surface 20a by the reference c_4. The distance c_4 is larger than the distance c_3. The clothing 14d of the card flat bars 14^{IV}, 14^{V}, 14^{VI} subtends a respective acute angle β with the tangent to the cylinder clothing 4a, with the result that the carding nip opens out in the direction of rotation 4b of the high-speed cylinder 4. The distance between the clothing 14d and the cylinder clothing 4a is denoted at the entry of the carding nip by the letter a, and at the exit by the letter e, e being greater than a. The angle of inclination β is termed the so-called counter-offset angle. The slow-running card flat bars 14^{IV}, 14^{V}, 14^{VI} are located in the region of the card flat guide roller 13b, that is, in the region of the card flat entry or fibre outlet. Figs 3a and 3b serve to illustrate the adjustment of the offset angle and counter-offset angle. The pins 14b of identical diameters in Figs 3a and 3b can in practice instead be of the form corresponding to Figs 5a to 5c.

Please amend the paragraph starting at p. 16, line 4, as follows:

In the embodiment of Figs 5a to 5c, the card flat head consist of two sliding elements [[$14b^I$, $14b^{II}$,]] $14b_1$, $14b_2$, one end region of which is secured in apertures of the card flat heel part 14a (see

DE-A- 43 05 148). The sliding element [[14b^{II},]] 14b$_2$ is a cylindrical pin of stainless steel having a diameter of, for example, 6 mm; it projects beyond the end face of the card flat bar 14^{VI} by distance g. The other sliding element [[14b^{I}]] 14b$_1$ consists of a cylindrical pin 14.2 having a diameter of, for example, 6 mm, at the free end of which a circular disc 14.1 of stainless steel having a diameter of, for example, 18 mm, is mounted and projects beyond the end face of the card flat bar 14^{VI} by distance f. In place of the disc 14.1, the pin 14.2 can be angled, that is, bent towards the sliding-contact surface 21a. Distance f is larger than distance g. An elongate, flexible, curved carrier element 24 is arranged on the flexible bend 17, and can be displaced parallel to the flexible bend 17 and can be of wedge-form construction. On the upper side of the carrier element 24, the two curved slideways 20 and 21 of, for example, anti-friction plastics material, are arranged in a secure manner side by side. In operation, the sliding element [[14b^{II}]] 14b$_2$ slides on the sliding-contact surface 20a (see Figs 4a to 4c) of the slideway 20 and the disc 14.1 of the sliding element [[14b^{I}]] 14b$_1$ slides on the sliding-contact surface 21a (see Figs 4a to 4c) of the slideway 21.

Please amend the paragraph starting at p. 16, line 34, as follows:

Because the diameter d_1 of the disc 14.1 is larger than the diameter d_2 of the pin [[14b^{II}]] 14b$_2$ and the distance f is larger than the distance g, at the card flat entry the sliding element [[14b^{I}]] 14b$_1$ extends over the sliding-contact surface 20a to engage with the sliding-contact surface 21a arranged lower down. At the same time, the shorter sliding element [[14b^{II}]] 14b$_2$ engages with the sliding-contact surface 20a arranged higher up. In this way, the opening carding nip of angle β is formed. As the card flat bar 14^{IV} slides in direction C, at the card flat exit the sliding element [[14b]]

$14b_2$, having slid beyond the intersection point of the two sliding-contact surfaces 20a, 21a, engages with the now lower sliding-contact surface 20a and the disc 14.1 engages with the higher sliding-contact surface 21a. By angling the card bars, the closing carding nip of angle α is formed at the card flat exit.